UNIVERSITY OF
KWAZULU-NATAL
INYUVESI
YAKWAZULU-NATALI

SCHOOL OF ENGINEERING

EXAMINATIONS: NOVEMBER 2018

COURSE AND CODE: CHEMICAL ENGINEERING PRINCIPLES 2 ENCH1EB

DURATION: 2 HOURS

TOTAL MARKS: 100

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INTERNAL MODERATOR: MRS A SINGH

EXTERNAL MODERATOR: DR SL KIAMBI

INSTRUCTIONS:

1. **ALL** questions should be attempted.
2. Any programmable or non-programmable calculator may be used provided it has been cleared of any information that would subvert the purpose of the examination.
3. Calculations must be shown in sufficient detail to illustrate your understanding of the procedure.
4. **Two answer books are provided. Label them Book A and Book B. Answer Section A in Book A (NM – Mass Balancing) and Section B in Book B (PN – Energy Balancing).**

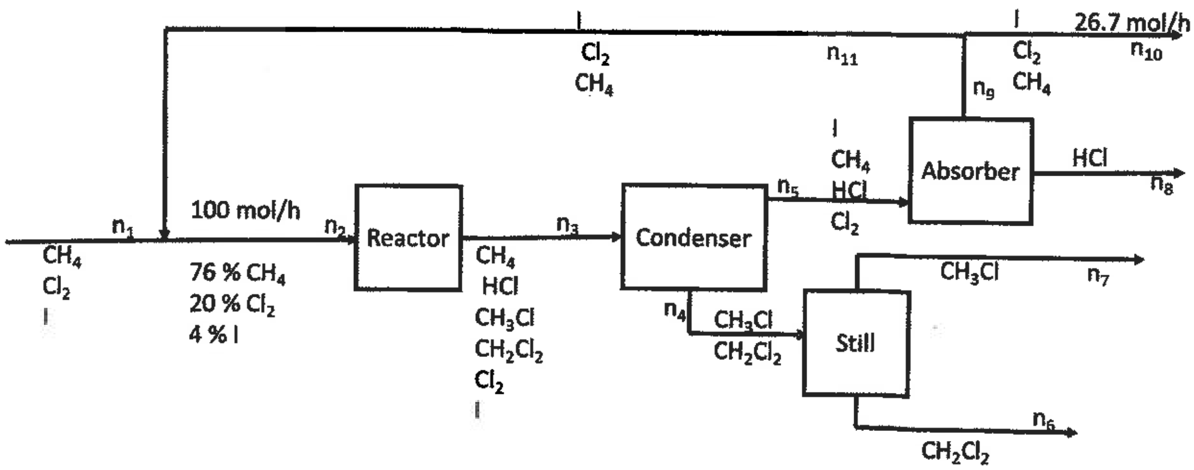
SECTION A

QUESTION 1

Methane reacts with chlorine to produce methyl chloride (CH_3Cl - desired product) and hydrogen chloride, as shown in reaction (R-1). Once formed, the methyl chloride may undergo further chlorination to form methylene chloride (CH_2Cl_2 - undesired chemical), shown in reaction (R-2).

$$CH_4 + Cl_2 \rightarrow CH_3Cl + HCl \qquad (R-1)$$
$$CH_3Cl + Cl_2 \rightarrow CH_2Cl_2 + HCl \qquad (R-2)$$

A methyl chloride production process consists of a reactor, a condenser, a distillation column, and an absorption column. A gas stream (n_2 = *100 mol/h*) containing 76 mole% methane 20 mole % chlorine and the balance Inert (I) is fed to the reactor. In the reactor, a single-pass chlorine conversion of 90 % is attained. The flowrate of the methylene chloride (CH_2Cl_2) stream (n_6) is 2.57 mol/h and the mole ratio of methyl chloride to methylene chloride in the reactor effluent (n_3) is 5:1. The molar flow rate for the purge stream (n_{10}) is 26.70 mol/h.



a) Determine the molar flow rate of the **total** methyl chloride produced. (4)

b) Calculate the molar flow rates of hydrochloric acid, chlorine, inert and methane in the reactor effluent (n_3). (8)

c) Determine the molar flow rates of methane, chlorine and inert in the fresh feed (n_1). (13)

d) What is the overall conversion of chlorine? (4)

e) What is the selectivity of methyl chloride formation? (2)

f) Define the yield and calculate the yield of methyl chloride? (2)

TOTAL /33/

QUESTION 2

Butane is burned with air. No carbon monoxide is present in the combustion products.

$$C_4H_{10} + {}^{13}/_{2}\, O_2 \rightarrow 4CO_2 + 5H_2O$$

a) Draw a flowchart of the process described above.

(3)

b) Using a basis of 100 mol/s of butane, calculate the molar flow rate of all the exit gases when there is 90% butane conversion and air is 20% in excess.

(11)

c) What is the mole fraction of nitrogen in the exit stream?

(3)

TOTAL /17/

SECTION B

QUESTION 3

A vessel of volume 0.04 m^3 contains wet steam at a temperature of 250.3 °C. The mass of the liquid water present is 9 kg.

i) What is the pressure?

(1)

ii) Calculate the mass of the wet mixture.

(5)

iii) Calculate the specific volume and enthalpy of the mixture.

(9)

TOTAL /15/

DATA
Steam tables are provided on **PAGES 7 to 9.**

QUESTION 4

The hydrogenation of benzene to cyclohexane is an important large-scale chemical process. Cyclohexane is a relatively stable cycloalkane and on a commercial scale, cyclohexane production is mostly based on the catalytic hydrogenation of benzene, which can be conducted in the liquid or vapor phase in the presence of hydrogen. For the reaction, vaporised benzene is mixed with hydrogen and passed over a packed bed with a nickel-based catalyst. The reaction (R1) is conducted at a temperature of 150 - 300°C. Higher temperatures can lead to thermodynamic limitations on benzene conversion, thermal cracking and increased by-product. Nitrogen is the inert component of the reaction mixture.

$$C_6H_6\,(g) + 3H_2\,(g) \rightarrow C_6H_{12}\,(g) \qquad \text{(Reaction 1)}$$

i. Calculate the standard heat of reaction, $\Delta\hat{H}^0_{r1}$

(2)

ii. Calculate the heat of reaction, $\Delta\hat{H}_{r1}$, at 150 °C.

(10)

Suppose that benzene and hydrogen, in a molar ratio of 1:5, at 150 °C, is fed to the reactor. The molar ratio of nitrogen to the combined feed is 1:1. The conversion is 70 %.

iii. For a feed rate of 100 kmol/h of benzene, calculate the composition of the product stream.

(10)

iv. The product stream is cooled from 150 °C to 80 °C at 1 atm. Calculate the cooling rate in (kW).

(10)

v. Consider the components cyclohexane and benzene in the product stream. Will it be easy to separate these two components in a distillation column to recover the product, cyclohexane? Comment.

(3)

TOTAL /35/

DATA provided on the next page.

Table 2. Physical property data

Compound	Benzene	Hydrogen	Cyclohexane	Nitrogen
Formulae	C_6H_6	H_2	C_6H_{12}	N_2
Mol. Wt.	78.11	2.016	84.16	28.08
SG (20°/4°)	0.879	-	0.783	-
T_m (°C)[a]	5.53	-259.19	6.54	-210.0
$\Delta\hat{H}_m(T_m)$ kJ/mol	9.837	0.12	2.34	0.720
T_b (°C)[a]	80.09	-256.76	80.72	-195.8
$\Delta\hat{H}_{vap}(T_b)$ kJ/mol	30.71	0.904	29.87	5.577
$\Delta\hat{H}_f^o$ kJ/mol	48.66 (l); 82.93 (g)	0 (g)	-157.65 (l); -123.2 (g)	0 (g)

[a]Boiling point at 1 atm.

Table 3. Heat Capacities

C_p (J/mol.°C) or (J/mol.K) = $a + bT + cT^2 + dT^3$ [T in °C]

Compound	Benzene	Hydrogen	Cyclohexane	Nitrogen
Formulae	C_6H_6	H_2	C_6H_{12}	N_2
Mol. Wt.	64.07	80.07	32.00	28.08
State	g	g	g	g
a	74.06	28.84	94.140	29.00
$b.10^2$	32.95	0.00765	49.62	0.2199
$c.10^5$	-25.20	0.3288	-31.90	0.5723
$d.10^9$	77.57	-0.8698	80.63	-2.871
T range (units of T)	0-1200	0-1500	0-1200	0-1500

DATA continued on the next page.

Table 4. Constant Heat Capacities

Compound	**Benzene**	**Cyclohexane**
Formulae	C_6H_6	C_6H_{12}
Mol. Wt.	64.07	32.00
State	l	l
C_p (J/mol.°C) or (J/mol.K)	118.4	156.5

P(bar)	T(°C)	$\hat{V}$(m³/kg) Water	$\hat{V}$(m³/kg) Steam	$\hat{U}$(kJ/kg) Water	$\hat{U}$(kJ/kg) Steam	$\hat{H}$(kJ/kg) Water	$\hat{H}$(kJ/kg) Evaporation	$\hat{H}$(kJ/kg) Steam
36	244.2	0.001238	0.0554	1053.1	2602.2	1057.6	1744.2	2801.7
38	247.3	0.001245	0.0524	1068.0	2601.9	1072.7	1728.4	2801.1
40	250.3	0.001252	0.0497	1082.4	2601.3	1087.4	1712.9	2800.3
42	253.2	0.001259	0.0473	1096.3	2600.7	1101.6	1697.8	2799.4
44	256.0	0.001266	0.0451	1109.8	2599.9	1115.4	1682.9	2798.3
46	258.8	0.001272	0.0430	1122.9	2599.1	1128.8	1668.3	2797.1
48	261.4	0.001279	0.0412	1135.6	2598.1	1141.8	1653.9	2795.7
50	263.9	0.001286	0.0394	1148.0	2597.0	1154.5	1639.7	2794.2
52	266.4	0.001292	0.0378	1160.1	2595.9	1166.8	1625.7	2792.6
54	268.8	0.001299	0.0363	1171.9	2594.6	1178.9	1611.9	2790.8
56	271.1	0.001306	0.0349	1183.5	2593.3	1190.8	1598.2	2789.0
58	273.3	0.001312	0.0337	1194.7	2591.9	1202.3	1584.7	2787.0
60	275.6	0.001319	0.0324	1205.8	2590.4	1213.7	1571.3	2785.0
62	277.7	0.001325	0.0313	1216.6	2588.8	1224.8	1558.0	2782.9
64	279.8	0.001332	0.0302	1227.2	2587.2	1235.7	1544.9	2780.6
66	281.8	0.001338	0.0292	1237.6	2585.5	1246.5	1531.9	2778.3
68	283.8	0.001345	0.0283	1247.9	2583.7	1257.0	1518.9	2775.9
70	285.8	0.001351	0.0274	1258.0	2581.8	1267.4	1506.0	2773.5
72	287.7	0.001358	0.0265	1267.9	2579.9	1277.6	1493.3	2770.9
74	289.6	0.001364	0.0257	1277.6	2578.0	1287.7	1480.5	2768.3
76	291.4	0.001371	0.0249	1287.2	2575.9	1297.6	1467.9	2765.5
78	293.2	0.001378	0.0242	1296.7	2573.8	1307.4	1455.3	2762.8
80	295.0	0.001384	0.0235	1306.0	2571.7	1317.1	1442.8	2759.9
82	296.7	0.001391	0.0229	1315.2	2569.5	1326.6	1430.3	2757.0
84	298.4	0.001398	0.0222	1324.3	2567.2	1336.1	1417.9	2754.0
86	300.1	0.001404	0.0216	1333.3	2564.9	1345.4	1405.5	2750.9
88	301.7	0.001411	0.0210	1342.2	2562.6	1354.6	1393.2	2747.8

Table 1. Properties of saturated steam: Pressure Table

90	303.3	0.001418	0.02050	1351.0	2560.1	1363.7	1380.9	2744.6
92	304.9	0.001425	0.01996	1359.7	2557.7	1372.8	1368.6	2741.4
94	306.4	0.001432	0.01945	1368.2	2555.2	1381.7	1356.3	2738.0
96	308.0	0.001439	0.01897	1376.7	2552.6	1390.6	1344.1	2734.7
98	309.5	0.001446	0.01849	1385.2	2550.0	1399.3	1331.9	2731.2
100	311.0	0.001453	0.01804	1393.5	2547.3	1408.0	1319.7	2727.7
105	314.6	0.001470	0.01698	1414.1	2540.4	1429.5	1289.2	2718.7
110	318.0	0.001489	0.01601	1434.2	2533.2	1450.6	1258.7	2709.3
115	321.4	0.001507	0.01511	1454.0	2525.7	1471.3	1228.2	2699.5
120	324.6	0.001527	0.01428	1473.4	2517.8	1491.8	1197.4	2689.2
125	327.8	0.001547	0.01351	1492.7	2509.4	1512.0	1166.4	2678.4
130	330.8	0.001567	0.01280	1511.6	2500.6	1532.0	1135.0	2667.0
135	333.8	0.001588	0.01213	1530.4	2491.3	1551.9	1103.1	2655.0
140	336.6	0.001611	0.01150	1549.1	2481.4	1571.6	1070.7	2642.4
145	339.4	0.001634	0.01090	1567.5	2471.0	1591.3	1037.7	2629.1
150	342.1	0.001658	0.01034	1586.1	2459.9	1611.0	1004.0	2615.0
155	344.8	0.001683	0.00981	1604.6	2448.2	1630.7	969.6	2600.3
160	347.3	0.001710	0.00931	1623.2	2436.0	1650.5	934.3	2584.9
165	349.8	0.001739	0.00883	1641.8	2423.1	1670.5	898.3	2568.8
170	352.3	0.001770	0.00837	1661.6	2409.3	1691.7	859.9	2551.6
175	354.6	0.001803	0.00793	1681.8	2394.6	1713.3	820.0	2533.3
180	357.0	0.001840	0.00750	1701.7	2378.9	1734.8	779.1	2513.9
185	359.2	0.001881	0.00708	1721.7	2362.1	1756.5	736.6	2493.1
190	361.4	0.001926	0.00668	1742.1	2343.8	1778.7	692.0	2470.6
195	363.6	0.001977	0.00628	1763.2	2323.6	1801.8	644.2	2446.0
200	365.7	0.00204	0.00588	1785.7	2300.8	1826.5	591.9	2418.4
205	367.8	0.00211	0.00546	1810.7	2274.4	1853.9	532.5	2386.4
210	369.8	0.00220	0.00502	1840.0	2242.1	1886.3	461.3	2347.6
215	371.8	0.00234	0.00451	1878.6	2198.1	1928.9	366.2	2295.2
220	373.7	0.00267	0.00373	1952	2114	2011	185	2196
221.2 (Critical point)	374.15	0.00317	0.00317	2038	2038	2108	0	2108

Table 1. Properties of saturated steam: Pressure Table

Table 2. Properties of superheated steam

P(bar) (T_{sat}, °C)		Sat'd Water	Sat'd Steam	Temperature (°C)→ 50	75	100	150	200	250	300	350
0.0	$\hat{H}$	—	—	2595	2642	2689	2784	2880	2978	3077	3177
(—)	$\hat{U}$	—	—	2446	2481	2517	2589	2662	2736	2812	2890
	$\hat{V}$	—	—	—	—	—	—	—	—	—	—
0.1	$\hat{H}$	191.8	2584.8	2593	2640	2688	2783	2880	2977	3077	3177
(45.8)	$\hat{U}$	191.8	2438.0	2444	2480	2516	2588	2661	2736	2812	2890
	$\hat{V}$	0.00101	14.7	14.8	16.0	17.2	19.5	21.8	24.2	26.5	28.7
0.5	$\hat{H}$	340.6	2646.0	209.3	313.9	2683	2780	2878	2979	3076	3177
(81.3)	$\hat{U}$	340.6	2484.0	209.2	313.9	2512	2586	2660	2735	2811	2889
	$\hat{V}$	0.00103	3.24	0.00101	0.00103	3.41	3.89	4.35	4.83	5.29	5.75
1.0	$\hat{H}$	417.5	2675.4	209.3	314.0	2676	2776	2875	2975	3074	3176
(99.6)	$\hat{U}$	417.5	2506.1	209.2	313.9	2507	2583	2658	2734	2811	2889
	$\hat{V}$	0.00104	1.69	0.00101	0.00103	1.69	1.94	2.17	2.40	2.64	2.87
5.0	$\hat{H}$	640.1	2747.5	209.7	314.3	419.4	632.2	2855	2961	3065	3168
(151.8)	$\hat{U}$	639.6	2560.2	209.2	313.8	418.8	631.6	2643	2724	2803	2883
	$\hat{V}$	0.00109	0.375	0.00101	0.00103	0.00104	0.00109	0.425	0.474	0.522	0.571
10	$\hat{H}$	762.6	2776.2	210.1	314.7	419.7	632.5	2827	2943	3052	3159
(179.9)	$\hat{U}$	761.5	2582	209.1	313.7	418.7	631.4	2621	2710	2794	2876
	$\hat{V}$	0.00113	0.194	0.00101	0.00103	0.00104	0.00109	0.206	0.233	0.258	0.282
20	$\hat{H}$	908.6	2797.2	211.0	315.5	420.5	633.1	852.6	2902	3025	3139
(212.4)	$\hat{U}$	906.2	2598.2	209.0	313.5	418.4	603.9	850.2	2679	2774	2862
	$\hat{V}$	0.00118	0.09950	0.00101	0.00102	0.00104	0.00109	0.00116	0.111	0.125	0.139
40	$\hat{H}$	1087.4	2800.3	212.7	317.1	422.0	634.3	853.4	1085.8	2962	3095
(250.3)	$\hat{U}$	1082.4	2601.3	208.6	313.0	417.8	630.0	848.8	1080.8	2727	2829
	$\hat{V}$	0.00125	0.04975	0.00101	0.00102	0.00104	0.00109	0.00115	0.00125	0.0588	0.0665
60	$\hat{H}$	1213.7	2785.0	214.4	318.7	423.5	635.6	854.2	1085.8	2885	3046
(275.6)	$\hat{U}$	1205.8	2590.4	208.3	312.6	417.3	629.1	847.3	1078.3	2668	2792
	$\hat{V}$	0.00132	0.0325	0.00101	0.00103	0.00104	0.00109	0.00115	0.00125	0.0361	0.0422
80	$\hat{H}$	1317.1	2759.9	216.1	320.3	425.0	636.8	855.1	1085.8	2787	2990
(295.0)	$\hat{U}$	1306.0	2571.7	208.1	312.3	416.7	628.2	845.9	1075.8	2593	2750
	$\hat{V}$	0.00139	0.0235	0.00101	0.00102	0.00104	0.00109	0.00115	0.00124	0.0243	0.0299
100	$\hat{H}$	1408.0	2727.7	217.8	322.9	426.5	638.1	855.9	1085.8	1343.4	2926
(311.0)	$\hat{U}$	1393.5	2547.3	207.8	311.7	416.1	627.3	844.4	1073.4	1329.4	2702
	$\hat{V}$	0.00145	0.0181	0.00101	0.00102	0.00104	0.00109	0.00115	0.00124	0.00140	0.0224
150	$\hat{H}$	1611.0	2615.0	222.1	326.0	430.3	641.3	858.1	1086.2	1338.2	2695
(342.1)	$\hat{U}$	1586.1	2459.9	207.0	310.7	414.7	625.0	841.0	1067.7	1317.6	2523
	$\hat{V}$	0.00166	0.0103	0.00101	0.00102	0.00104	0.00108	0.00114	0.00123	0.00138	0.0115
200	$\hat{H}$	1826.5	2418.4	226.4	330.0	434.0	644.5	860.4	1086.7	1334.3	1647.1
(365.7)	$\hat{U}$	1785.7	2300.8	206.3	309.7	413.2	622.9	837.7	1062.2	1307.1	1613.7
	$\hat{V}$	0.00204	0.005875	0.00100	0.00102	0.00103	0.00108	0.00114	0.00122	0.00136	0.00167
221.2(P_c)	$\hat{H}$	2108	2108	228.2	331.7	435.7	645.8	861.4	1087.0	1332.8	1635.5
(374.15)(T_c)	$\hat{U}$	2037.8	2037.8	206.0	309.2	412.8	622.0	836.3	1060.0	1302.9	1600.3
	$\hat{V}$	0.00317	0.00317	0.00100	0.00102	0.00103	0.00108	0.00114	0.00122	0.00135	0.00163
250	$\hat{H}$	—	—	230.7	334.0	437.8	647.7	862.8	1087.5	1331.1	1625.0
(—)	$\hat{U}$	—	—	205.7	308.7	412.1	620.8	834.4	1057.0	1297.5	1585.0
	$\hat{V}$	—	—	0.00100	0.00101	0.00103	0.00108	0.00113	0.00122	0.00135	0.00160
300	$\hat{H}$	—	—	235.0	338.1	441.6	650.9	865.2	1088.4	1328.7	1609.9
(—)	$\hat{U}$	—	—	205.0	307.7	410.8	618.7	831.3	1052.1	1288.7	1563.3
	$\hat{V}$	—	—	0.0009990	0.00101	0.00103	0.00107	0.00113	0.00121	0.00133	0.00155
500	$\hat{H}$	—	—	251.9	354.2	456.8	664.1	875.4	1093.6	1323.7	1576.3
(—)	$\hat{U}$	—	—	202.4	304.0	405.8	611.0	819.7	1034.3	1259.3	1504.1
	$\hat{V}$	—	—	0.0009911	0.00100	0.00102	0.00106	0.00111	0.00119	0.00129	0.00144
1000	$\hat{H}$	—	—	293.9	394.3	495.1	698.0	903.5	1113.0	1328.7	1550.5
(—)	$\hat{U}$	—	—	196.5	295.7	395.1	594.4	795.3	999.0	1207.1	1419.0
	$\hat{V}$	—	—	0.0009737	0.0009852	0.001000	0.00104	0.00108	0.00114	0.00122	0.00131